

# On the Way to Plankton Net Calibration

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## Outline

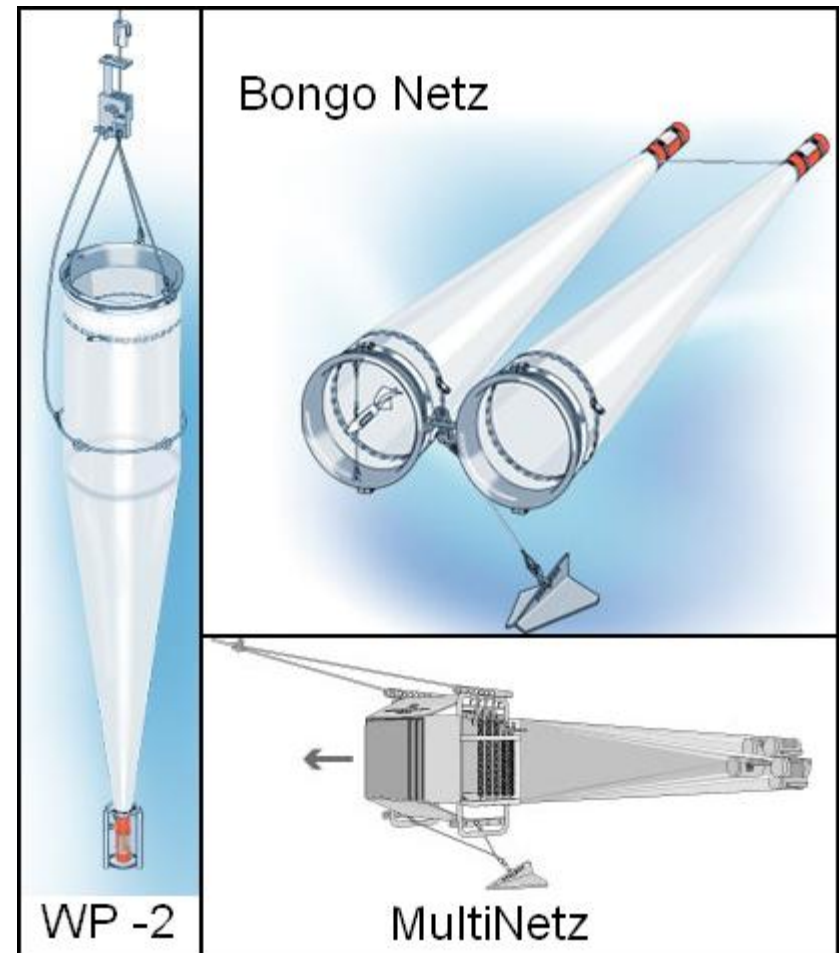
- Introduction
- Methods
- Results
- Conclusion
- Future Work

## Introduction

- Zooplankton is an important link in the marine food chain. It connects lower trophic levels like algae with higher trophic levels like fish.
- To identify global synchronies in zooplankton populations a need for intercalibration to document gear and sampling differences arose.

➔ Investigate hydrodynamic properties in an appropriate testing facility, or

➔ use computational fluid dynamics (CFD) methods.





## Introduction

Investigate the hydrodynamics of plankton nets with CFD methods.

- Predict the flow patterns around and through plankton nets with Reynolds averaged Navier-Stokes (RANS) methods.
- Assess the method by comparing CFD results with experimental flow investigations done by Tranter & Heron (1968) and Enerhaug (2005).



## Methods

- RANS methods provide time-averaged information about flow properties
- ➔ A constant towing velocity was ensured during measurements in the testing facilities and,
- ➔ clogging effects were not considered.

## Methods - Problems to face

- Nets are flexible structures
- Mesh opening is too small to model each mesh (max. mesh opening approx. 0.5 mm)

Weights are used, e. g. WP-2 net:

25 kg lead weight at the end.

↳ Assumption: nets are rigid.



Physical properties of the gauze are simulated by defining a directional pressure loss over a porous body representing the gauze.



## Methods - Flows in porous media

$$\frac{\partial \bar{u}_i}{\partial t} + \frac{\partial \bar{u}_i \bar{u}_j}{\partial x_j} = \bar{f}_i - \frac{1}{\rho} \frac{\partial \bar{p}}{\partial x_i} + \nu \cdot \frac{\partial^2 \bar{u}_i}{\partial x_j^2} - \frac{\partial (\overline{u_i' u_j'})}{\partial x_j} + S_i,$$

$$S_i = -C_{R1i} \cdot u_i - C_{R2i} \cdot |u_i| \cdot u_i$$

$C_{R1i}$  – linear resistance coefficient

$C_{R2i}$  – quadratic resistance coefficient

$u_i$  – superficial velocity

Ansys CFX directional loss model requires  $C_{R1}$  and  $C_{R2}$  in the streamwise direction



## Methods - Directional pressure loss

- Magnitude of the pressure loss ( $C_{R1}$ ,  $C_{R2}$ )?
- Direction of flow out of the gauze?

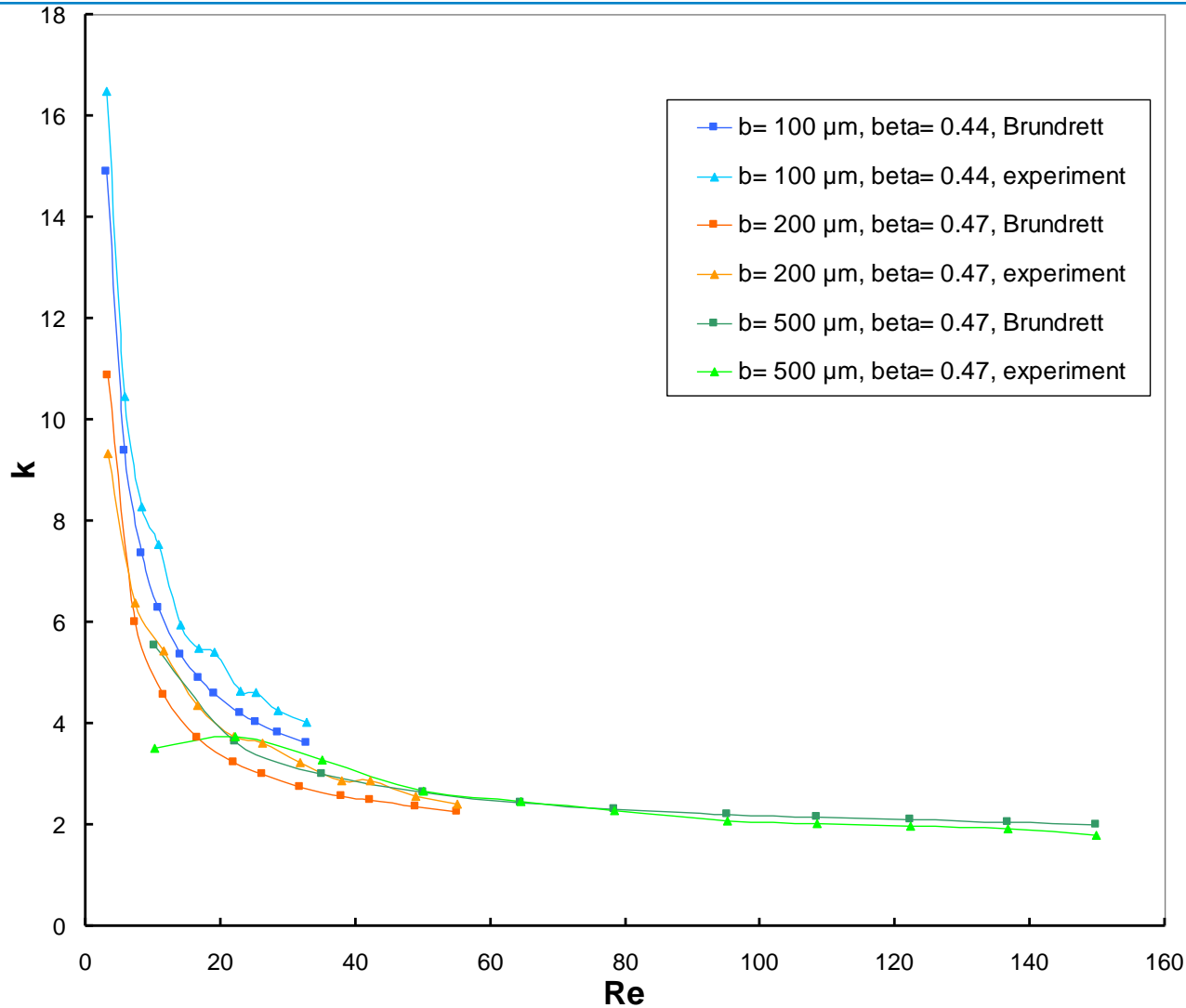




## Methods - Directional pressure loss

Pressure loss over gauze screens perpendicular to the flow

- Experimental data
- E. Brundrett, 1993 - formula to calculate the pressure loss over gauze screens



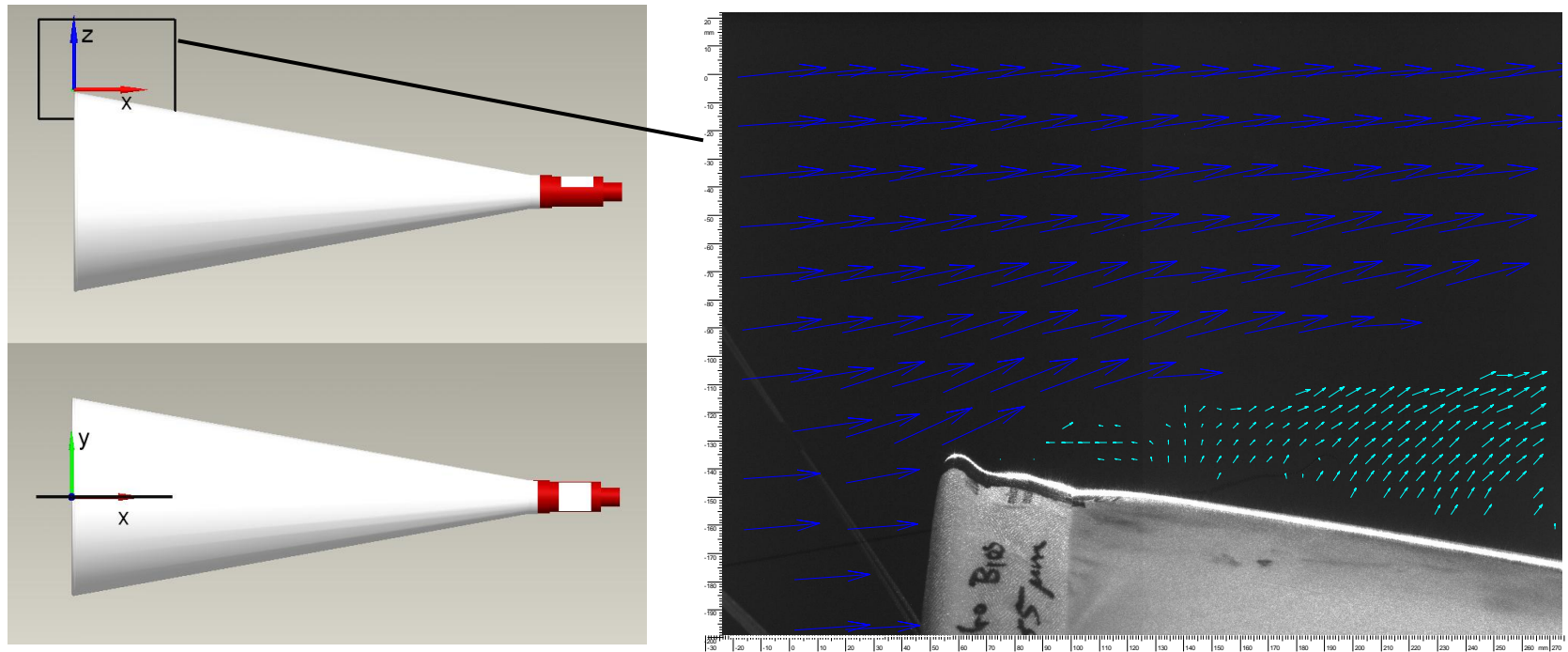
$$k = \frac{\overline{\Delta p}}{\frac{1}{2} \rho \cdot u_0^2}$$

$$Re = \frac{u_0 \cdot d}{\nu}$$

## Methods - Directional pressure loss

A. J. Reynolds, 1969 – porosity less than 0.5  $\Rightarrow$  direction of outflow normal to the gauze screen

Results of Particle Image Velocimetry (PIV) System - measurements





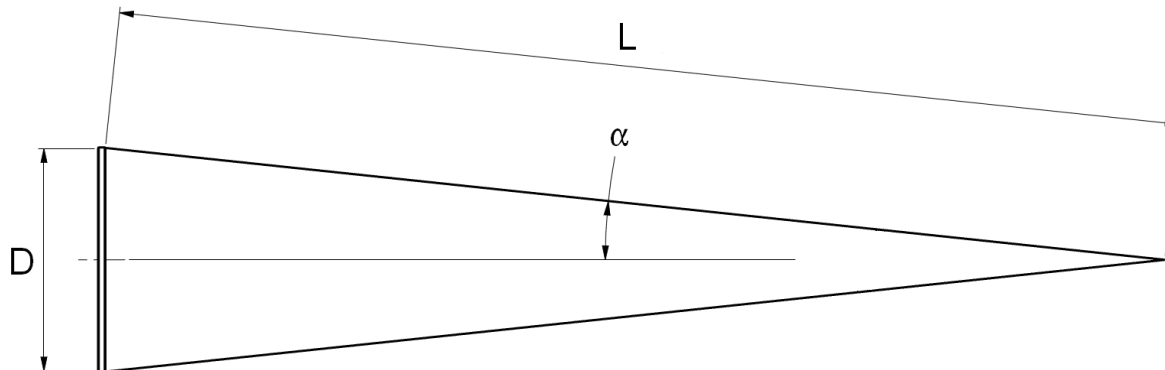
## Methods - Directional pressure loss

### Assumptions

- Nets are rigid
- Pressure loss is predicted by the formula given by Brundrett
- Direction of flow out of gauze normal to the gauze

## Methods - Test objects

| net                | abbreviation | mouth diameter (D) in m | length of side (L) in m | taper angle ( $\alpha$ ) in deg. | mesh opening (b) in $\mu\text{m}$ | Twine diameter (d) in $\mu\text{m}$ | Porosity ( $\beta$ ) |
|--------------------|--------------|-------------------------|-------------------------|----------------------------------|-----------------------------------|-------------------------------------|----------------------|
| prototype WP-2 net | N22          | 0.67                    | 2.42                    | 6.3                              | 210                               | 90                                  | 0.49                 |
| Enerhaug model 1.4 | E14          | 0.8                     | 1.56                    | 15                               | 500                               | 230                                 | 0.47                 |
| Enerhaug model 3.1 | E31          | 0.8                     | 3.85                    | 6                                | 950                               | 305                                 | 0.57                 |
| Enerhaug model 3.2 | E32          | 0.8                     | 3.85                    | 6                                | 143                               | 153                                 | 0.23                 |

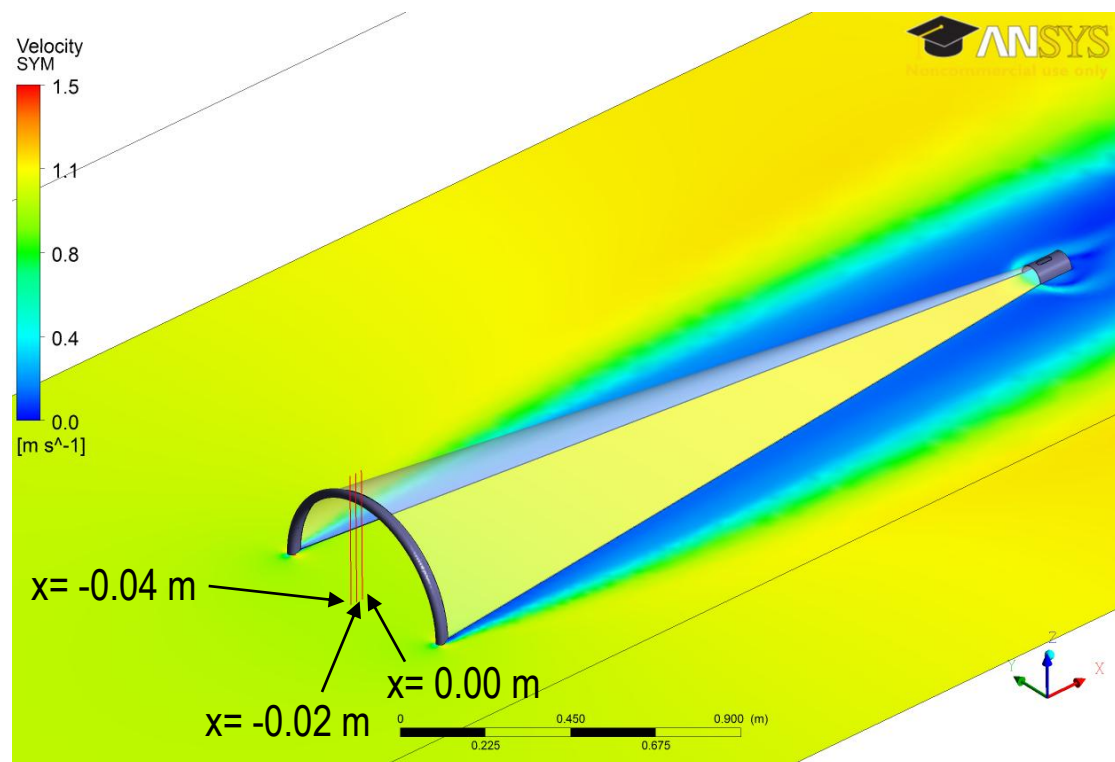




## Results

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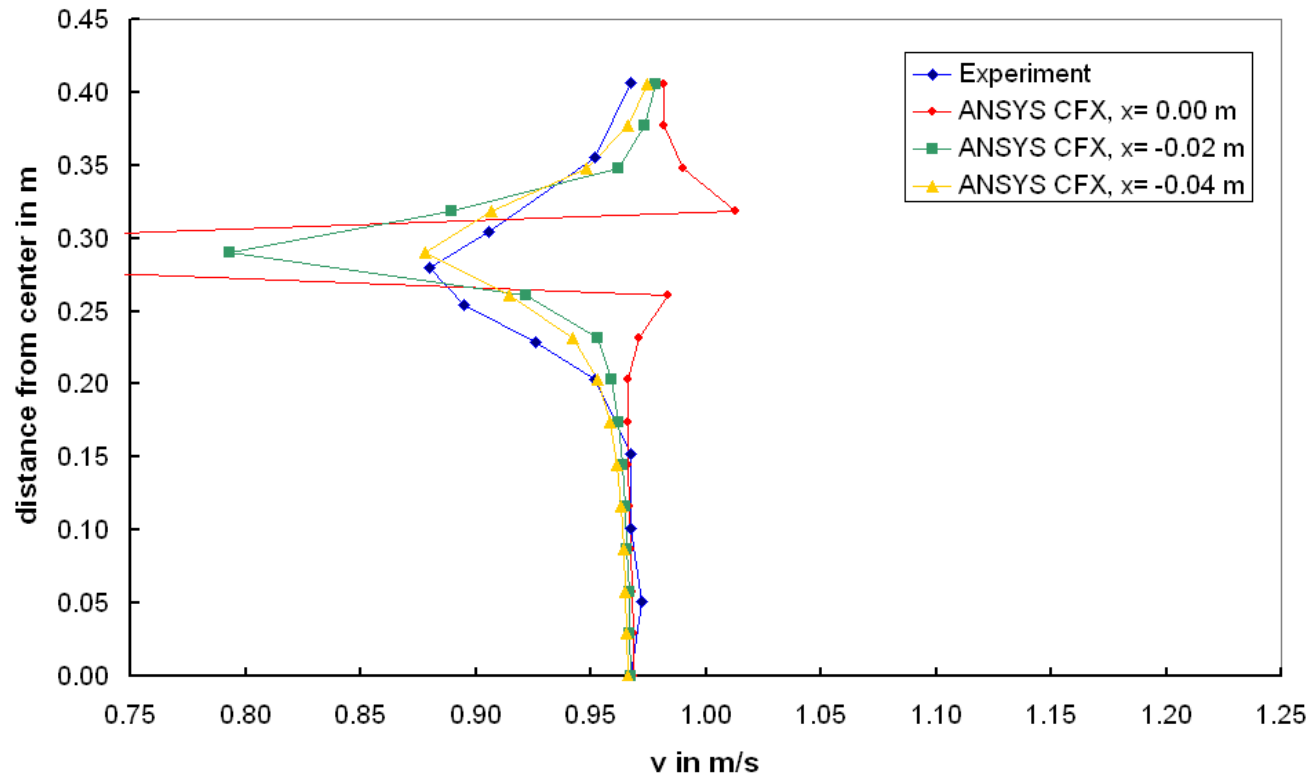
Simulation of prototyp WP-2 Net, Tranter & Heron „Zooplankton sampling“, UNESCO report 1968.





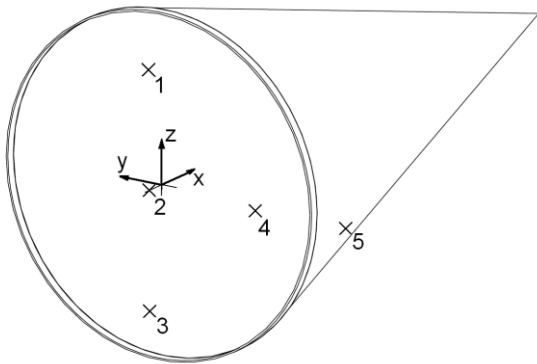
## Results

The prototype WP-2 net



## Results

Enerhaug nets: E14, E31, E32

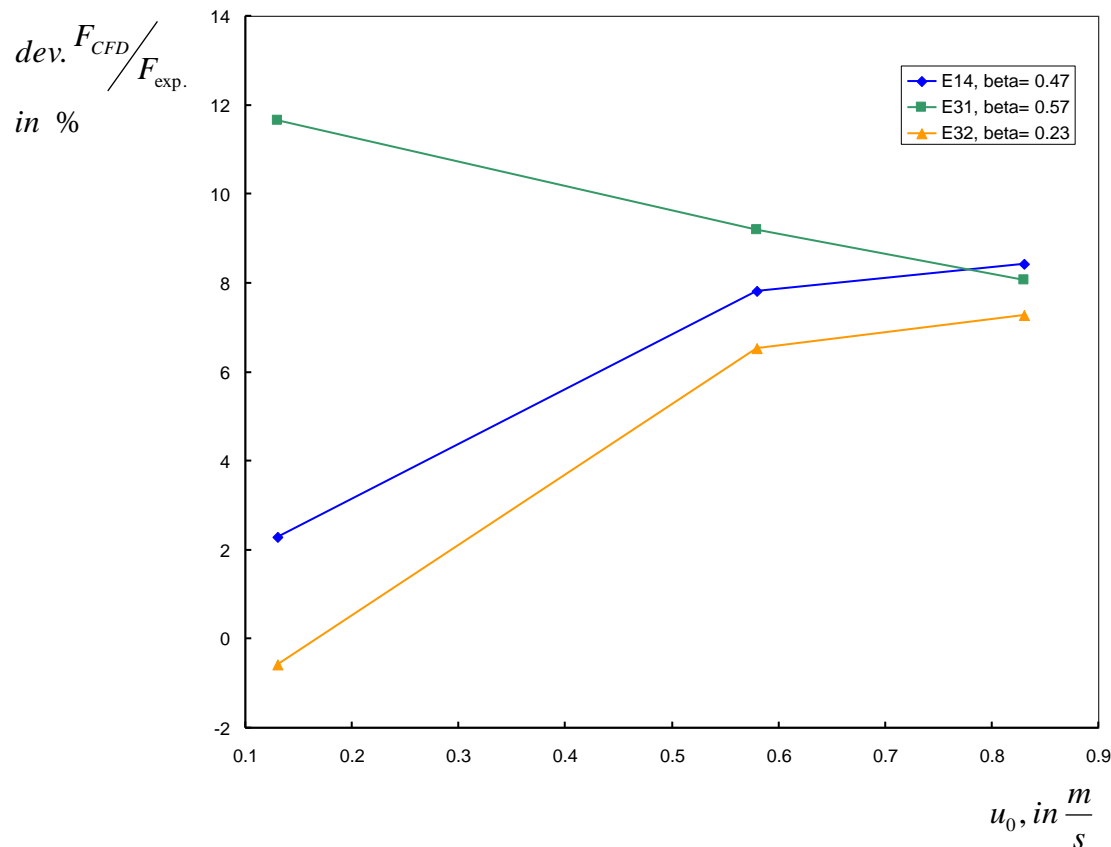


Volume flow rate  $Q$  into the net, based on Enerhaug

$$Q_{net} = \frac{(u_1 + u_3 + u_4)}{3} \cdot A_{mouth}$$

## Results

Enerhaug nets: E14, E31, E32



$$F = \frac{Q_{net}}{Q_{theory}} = \frac{Q_{net}}{u_0 \cdot A_{mouth}}$$

$F$  – filtration efficiency

$Q$  – volume flow rate

$u_0$  – approach velocity

$A_{mouth}$  – mouth area net

$\beta$  – porosity of gauze

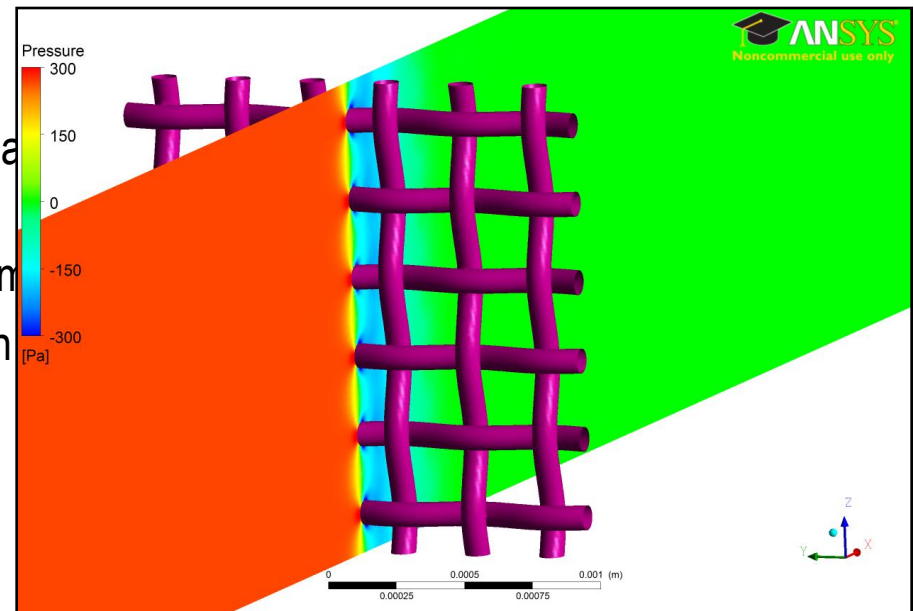


## Conclusion

- Promising results about the application of RANS methods to predict the hydrodynamics of plankton nets have been obtained.
- Deviations up to 13% occurred, on average 7 %.
- Weak point of the simulation is its simplification of the gauze assumed as a porous body.

## Future work

- Investigate the flow through inclined gas exchange devices in experiments and simulations
- Find a way to describe the hydrodynamic behavior of inclined gas exchange devices
- Compare any kind of plankton net with other types of gas exchange devices





Thank you for your attention!